

METHOD AND SYSTEM FOR AUTOMATIC RAMAN GAIN CONTROL

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CROSS-REFERENCE TO RELATED APPLICATION

10 This application is related to the co-pending and
commonly-assigned application Ser. No. _____, filed
on same date herewith, by Paul Reepschlager, entitled
"Methods and System for Automatic Optical Fiber Type
Identification."

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FIELD OF INVENTION

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The present invention relates to fiber optics as well as
to measuring gain in amplified fiber optic spans.

BACKGROUND OF THE INVENTION

25 It is known in the art that one manner of obtaining
additional optical gain in an amplified fiber optic span
is by pumping the line fiber with high-energy photon (low
wavelength) lasers. In the resulting "Raman effect",
high-energy photons are absorbed by the fiber and may be
re-emitted in the form of stimulated emission in the
30 presence of longer wavelength photons, thus resulting in
amplification. The gain profile for the stimulated re-
transmission has a finite width. Signal gain across a
wide spectral profile may involve the superposition of
gain profiles for several Raman pumps.

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Using adequate pump wavelengths to provide gain across a signal band, a known model can be derived to predict the relative pump powers required to achieve a desired gain profile through pump gain profile superposition, while taking into account several secondary non-linear fiber optic effects as well.

In the prior art, a closed loop system has been employed which monitors system span profile parameters for gain derivation. The desired Raman gain is then estimated on the basis of a modeled solution. However, this implementation does not take into account the dynamic nature of the system span profiles. Consequently, in cases where the system span profiles are dynamic in nature, the known gain control model (algorithm) will fail. Furthermore, Raman gain estimation on the basis of a modeled solution often itself employs an open loop gain implementation, and the resulting gain profile is not corrected.

United States Patent 6,081,323 issued to Mahgerefteh et al. on June 27, 2000, teaches a method and apparatus for the measurement of Raman gain spectrum in an optical fiber. This patent, however, describes the determination of Raman gain spectrum and is silent on the measurement of Raman gain.

Therefore, there is a need for an improved method of calculating Raman gain which permits dynamic adjustments to system parameters, thus correcting gain inaccuracies induced by the application of known models and permitting an accurate derivation of the Raman gain.

SUMMARY OF INVENTION

Accordingly, it is an object of the invention to provide a closed loop control strategy using system wavelength
5 profile information to provide accurate derivation of Raman gain in a fiber optic span.

It is another object of the invention to provide a manner
10 in which Raman gain may be measured in real-time, in service.

The term "power profile" will be used herein as a generic term to describe either a gain profile or a loss profile.

15 According to one aspect of the invention, there is provided a method of dynamically determining a Raman gain profile of an optically amplified fiber optic span, said method comprising the steps of: measuring a power profile for each of a plurality of system components;
20 transmitting the measured power profiles to a central location; transmitting changes in the measured power profiles to the central location; and dynamically calculating the Raman gain profile for the system based on the changes in the measured power profiles.

25 According to another aspect of the invention, there is provided a system for dynamically determining a Raman gain profile of an optically amplified fiber optic span, said system comprising: optical spectrum analyzers for
30 measuring a power profile of said fiber optic span and of a plurality of system components so as to determine the existence of a loss or a gain therein; means for receiving the measured power profiles from the optical spectrum analyzers, and for receiving changes in the
35 measured power profiles; and means for dynamically

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calculating the Raman gain profile for the system based on the changes in the measured power profiles.

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BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the present invention will be further described with reference to the accompanying drawings, in which:

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Figure 1 illustrates diagrammatically a system for determining Raman gain in accordance with an embodiment of the present invention;

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Figure 2 illustrates diagrammatically a consideration of passive losses at the receiving end of a system according to Figure 1; and

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Figure 3 illustrates graphically individual pump wavelength profiles as well as a superposition of a single pump Raman gain profile in a system according to Figure 1.

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DETAILED DESCRIPTION OF THE INVENTION

The present invention postulates that, if collected in a central location, mapping information related to monitored wavelength profiles in a system can be utilized to derive the Raman gain within a span.

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Figure 1 illustrates a system for determining Raman gain in a fiber optic span in accordance with an embodiment of the present invention. Cost-effective optical spectrum

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analyzers (OSAs) 110 are provided in order to monitor wavelength power profiles, which permits the mapping of transmit and receive profiles within a fiber optic span 100. If collected at a central location, such as at processor 150, this mapping information may be utilized to derive the Raman gain within the span. In an embodiment of the present invention, the processor 150 is located at the receiving end of the span 100.

The following information is necessary in order to determine the spectral contribution (G3) of Raman pumps 140 incident on the receive amplifier 130: the originating profile (P1) of up-stream transmit amplifier 120; the loss profile (L2) for fiber optic span 100; and the profile (P4) measured at the input to the receive amplifier 130. The value of the Raman gain spectral contribution (G3) may be determined using the following equation:

$$P4(\lambda) = P1(\lambda) + G3(\lambda) - L2(\lambda), \text{ or}$$
$$G3(\lambda) = P4(\lambda) - P1(\lambda) + L2(\lambda)$$

Calculation of $G3(\lambda)$ is preferably performed at the receiving end. This calculation may be performed automatically by the processor 150, or by any other means capable of doing so. Alternatively, this calculation may be performed manually. Advantageously, the result of this calculation may be displayed on a display means 160.

Using this method in accordance with the present invention, the gain and ripple in the Raman gain profile will both be directly mapped as opposed to being estimated through reliance on model equations. The measurement of an actual spectral profile at the receive amplifier 130 by optical spectrum analyzer 110 permits

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pre-compensation of the Raman gain profile to be implemented and tracked with a high level of confidence.

Some level of inaccuracy may be expected in the derived Raman Gain profile. This inaccuracy will be manifested in OSNR (optical signal to noise ratio) results. Thus, as an outside loop in the control technique, a central body must be able to dictate Raman gain set-points across the spans to ensure that the end OSNR results are met.

The determination of the Raman gain using the above technique will only be effective if the dynamic nature of the transmit amplifier profile and the loss profile can be tracked.

First, consider changes in the transmit amplifier profile, $P_1(\lambda)$. To properly map the Raman gain profile, information about the profile $P_1(\lambda)$ of up-stream transmit amplifier 120 should be fed downstream to the receive amplifier 130. A continual spectral profile update strategy, however, may strain usage of an overhead channel 170. Therefore, in a preferred embodiment, it is proposed that only status updates be conveyed on a regular basis from the transmit amplifier. That is, once complete information about the transmit spectral profile $P_1(\lambda)$ has been conveyed to the receiver amplifier 130, regular message updates pertaining to the general operating conditions of the transmit amplifier 120 can advantageously be sent over the overhead channel 170. A tolerance band may be defined in the transmit amplifier profile $P_1(\lambda)$, within which minor localized changes in its output gain and ripple would not warrant a complete update of its spectral content information to the receive amplifier 130. Only under changes causing an "event" in the transmit amplifier's output operating profile would a

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complete profile update be sent. An event may be any one of: a profile change outside of the tolerance band, wavelength additions, loss of wavelengths, etc.

5 If congestion of the overhead channel momentarily detains communication of complete spectral updates from the transmit amplifier, then, in another embodiment, a method may be put in place to convey only basic information across the overhead channel (such as wavelength x has
10 been added with power y). Short term reliance on the open loop Raman amplifier model equations (resident with the Raman circuit pack) would be permitted to make limited independent adjustments to the Raman pumps 140 in order to accommodate transmitted profile changes. Closed
15 loop corrective measures may be implemented when the complete up-stream information can be conveyed across the overhead channel.

Next, consider changes in the fiber loss profile, $L_2(\lambda)$.
20 Any Raman gain derivation technique that treats the fiber loss profile as a static entity should cause some concern. Under such conditions, any degradation to the passive elements in the system (such as that due to temperature variations) would result in false estimates
25 of the Raman gain. Therefore, whether the fiber loss profile is initially procured through measurement techniques, or estimated based on typical fiber characteristics, this profile information will need to be dynamic, being updated periodically based on receive
30 amplifier OSA measurements.

The question remains: how can one determine whether changes have occurred within the span profile? According to the invention, the answer lies again in knowledge of
35 conditions in the rest of the span. Input spectral profile information can be measured at the receive

amplifier 130. If this input profile, $P4(\lambda)$, changes, but it is known that the booster output profile, $P1(\lambda)$, has remained consistent, and output power monitor conditions remain unchanged on the Raman pumps 140 (total power as well as individual pump powers), then the changes can be inferred to have occurred along the transmission medium.

Once the measurements of gain and loss profiles have been made, it is necessary to determine the change in the gain or loss profile. Two situations are discussed below: correction of the gain profile during initial system setup; and correction of the loss profile in service, when active parameters have not changed. First, the correction of gain profile during initial system set-up is considered. In initially setting up a span, there must be a preliminary understanding of system parameters in order to determine the amount of Raman gain required. In the present invention, a desired Raman gain profile can be chosen knowing the following values: the output of the transmit amplifier, $P1(\lambda)$; the desired profile at the receive amplifier input, $P4(\lambda)$; and an initial condition profile for the span loss, $L2(\lambda)$. A model is used to set the Raman pump powers to achieve the desired Raman gain profile, and the resulting measured gain will be:

$$G3_{measured}(\lambda) = P4_{measured}(\lambda) - P1_{known}(\lambda) + L2_{initial}(\lambda)$$

This may differ from the desired profile due to model errors for the Raman gain. Hence, initial offset adjustments can be made to the pump powers to achieve:

$$\begin{aligned} G3_{measured}(\lambda) &= G3_{desired}(\lambda) \\ &= P4_{measured}(\lambda) - P1_{known}(\lambda) + L2_{initial}(\lambda) \end{aligned}$$

It should be noted that the loss profile is assumed to be correct (due to measurement or due to inferred profile based on typical fiber characteristics). This is a necessary starting point.

Next, consideration is given to the correction of the loss profile in service, when active parameters have not changed. With any intended modification to the Raman gain profile, it must be assumed that the fiber loss profile is correct and static. This implies that, under steady state transmit amplifier and Raman amplifier operating conditions, the loss profile must be monitored and updated accordingly to account for environmental impacts upon it.

A change in the loss profile will be noticed as a change of the profile incident upon the receive amplifier. Under conditions wherein $P1(\lambda)$ has not changed and the Raman pumps are kept at a given operating point, changes in $P4(\lambda)$ may be attributed to a change in the loss of the transmission fiber $L2(\lambda)$. However, a change in $L2(\lambda)$ will result in a change in $G3(\lambda)$ through a change in the effective length of the Distributed Raman amplifier.

Therefore, before the change in fiber loss:

$$P4(\lambda) = P1(\lambda) + G3(\lambda) - L2(\lambda)$$

After the small change Δ in the received power at $P4$:

$$P4(\lambda) + \Delta(\lambda) = P1(\lambda) + G3(\lambda) - \delta_G(\lambda) - L2(\lambda) - \delta_L(\lambda)$$

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Where $\Delta(\lambda) = \delta_G(\lambda) + \delta_L(\lambda)$, and $\delta_G(\lambda)$ is the change in the Raman gain profile and $\delta_L(\lambda)$ is the change in the fiber loss spectrum and is much smaller than $L_2(\lambda)$.

5 Since it is very difficult to provide a simple method which (in low computational time) may determine $\delta_G(\lambda)$ and $\delta_L(\lambda)$, a simple linear approximation is used. As an initial supposition, consider $\delta_G(\lambda)$ as being very small compared to $\delta_L(\lambda)$. As such, since the entire change in
10 $P_4(\lambda)$ will be attributed to a change in the loss profile, $\delta_L(\lambda)$ can be calculated very easily ($\Delta_{\text{measured}}(\lambda) = \delta_L(\lambda)$). If the assumption is made that the change in fiber loss is equally distributed all along the transmission fiber, a change in the loss per unit length ($\Delta\alpha$) can be derived
15 from $\delta_L(\lambda)$.

As a second step in the analysis, it is then desirable to estimate the change in Raman gain occurring from the change in the fiber loss, since (as a counter to the
20 initial supposition) there does exist a finite change to $\delta_G(\lambda)$. In the linear regime, the Raman amplification depends only on three parameters: the Raman gain coefficient (C_r), the pumping power (P) and the absorption per unit length at the pumping wavelength (α).
25 In fact, it can be found that for a particular pump (i):

$$\delta_{G,i} = \frac{-4.343 C_{r,i} P_i \Delta\alpha}{\alpha_i^2}$$

30 C_r and P are constants in the present case, α is known from the previous iteration while $\Delta\alpha$ has been estimated previously. For a given signal wavelength, δ_G can then be estimated by adding the contribution from each pump.

The $\delta_L(\lambda)$ parameter can then be re-estimated by subtracting $\delta_G(\lambda)$ from the measured value $\Delta(\lambda)$:

$$\begin{aligned} L2(\lambda)_{\text{updated}} &= L2(\lambda)_{\text{previous}} + \delta_L(\lambda) \\ &= L2(\lambda)_{\text{previous}} + [\Delta(\lambda) - \delta_G(\lambda)] \end{aligned}$$

Since it is desirable to maintain a time-invariant profile into the receive amplifier, loss profile updates imply a need for Raman gain profile updates, since the Raman gain profile set-point is a function of the loss profile. Once adjustments to the Raman pump powers have been made to account for changes to the loss profile, the resultant gain profile measurement can be made:

$$G3_{\text{measured}}(\lambda) = P4_{\text{measured}}(\lambda) - P1_{\text{known}}(\lambda) + L2_{\text{updated}}(\lambda)$$

and corrective offset adjustments can be applied to the Raman pumps.

Updates to the loss profile and Raman Gain profile may be made regularly in incremental iterative steps.

In calculating the Raman gain, it is important to know if passive losses that may exist at the receiving end (i.e. patch panel loss, filter losses...) factor into the equation. If so, there is the potential for a large unknown offset on the measured gain.

Figure 2 is a modification of the concepts presented in earlier. Here an extra element 200, with a loss profile of C5 has been added to account for the static passive losses that will appear at the receiving end. Two other parameters are considered as well: $L2'$ and $P4'$. The profile $P4$, at the input of receive amplifier 130, is

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measured after the static losses, C5. The equivalent profile measurement without static losses is P4'. Since loss profile measurements, L2, will also be made at the input to the dual amplifier, the loss due to the fiber alone (without C5) is noted in the diagram as L2'. Raman gain, G3, needs to be defined as the actual gain derived by pumping the fiber. Hence, when setting up pump powers to deliver fiber gain, one should account for the additional static loss C5 (relatively easy to do with closed loop gain control).

Having defined parameters above, consider how the Raman gain is derived.

$$G3(\lambda) = P4(\lambda) - P1(\lambda) + L2(\lambda)$$

with P4 and L2 measured at the dual amplifier input.

But in this case, $L2(\lambda) = L2'(\lambda) + C5$ and $P4(\lambda) = P4'(\lambda) - C5$

Thus:

$$\begin{aligned} G3(\lambda) &= P4'(\lambda) + C5 - P1(\lambda) + L2'(\lambda) - C5 \\ &= P4'(\lambda) - P1(\lambda) + L2'(\lambda) \end{aligned}$$

Therefore, the calculation of G3 using measured parameters L2 and P4 is insensitive to the static losses on the receiving side.

Measurement of the loss profile can be effected under start of life, non-traffic-carrying conditions. If the transmit amplifier pumps are turned up to deliver superfluous (high power) Amplified Spontaneous Emission (ASE), this launched ASE profile could first be measured at the amplifier output using the OSA, and then measured

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at the receiving dual amplifier input. The difference between the profiles would be the mapping of the span loss profile.

5 As a first step, the Raman pump power settings need to be calculated relative to the fiber loss profile in order to achieve a specified Raman gain profile. For this reason, the fiber loss profile needs to be measured (or estimated by a typical value).

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As a second step, it is useful to determine the Raman gain spectrum provided by each pump. The combined Raman flat gain profile is the result of the superposition of several individual pump wavelength profiles, as
15 illustrated in Figure 3.

It is evident from Figure 3 that the shapes of the pump profiles must be known to permit an effective superposition. The shape is empirically determined, and
20 is dependent on fiber type.

A caveat lies in the reliability of using a pre-determined per-fiber-type typical Raman pump profile when implementing a solution. This use does not allow for
25 tolerance variations with same-type fibers. One solution to this problem is accomplished by measuring the pump profile on-site. Under the same start of life (traffic free) conditions used in determining the loss profile, each pump wavelength can be turned up independently, and
30 the resultant profile mapped at the receive amplifier. The resultant profile is derived through the difference between the ASE profile incident on the receiver amplifier before and after the Raman pump power application. This technique would be particularly
35 valuable in a situation wherein a foreign fiber type has previously been spliced into a span, and the typical

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profile for the dominant fiber type may not be applicable.

It was mentioned earlier, with respect to the correction
5 of gain profile during initial system set-up, that during
system initialization, the Raman gain model provides pump
set-points which may be non-optimal due to model
inaccuracies. That is, the resulting gain profile will
be measured through

$$G3_{\text{measured}}(\lambda) = P4_{\text{measured}}(\lambda) - P1_{\text{known}}(\lambda) + L2_{\text{initial}}(\lambda)$$

and this measured profile may not match the desired
profile. Pump offsets may be necessary to achieve:

$$G3_{\text{measured}}(\lambda) = G3_{\text{desired}}(\lambda)$$

Therefore, as a third step in the start of life
initialization procedure, it is possible to provide an
20 initial estimate of this offset to provide a first order
of correction to the model before traffic is activated
onto the link.

Under the transmitter amplifier ASE condition, if the
25 Raman pumps were then activated to provide a pre-
determined (modeled) gain, that resultant gain can be
measured at the receive amplifier. This provides a
method for comparing the gain provided by the model
against empirical observation.

30 Furthermore, if a link budget analysis has dictated that
the Raman gain within a span is to have a value Y, two
other gain values can be measured using the above
procedure, X being a value marginally below the desired
35 point, and Z being a value marginally above the desired

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point. The error between the set-point gain X and measured results can be obtained. Likewise, the error between the set-point gain Z and measured results can be obtained. From interpolation between these error

5 results, a linear function on the expected error in the gain Y can be found and used to first provide initial pump offsets on the model, and then for adjustment purposes.